Pressure Swing Absorption Device and Process for Separating CO₂ from Shifted Syngas and its Capture for Subsequent Storage

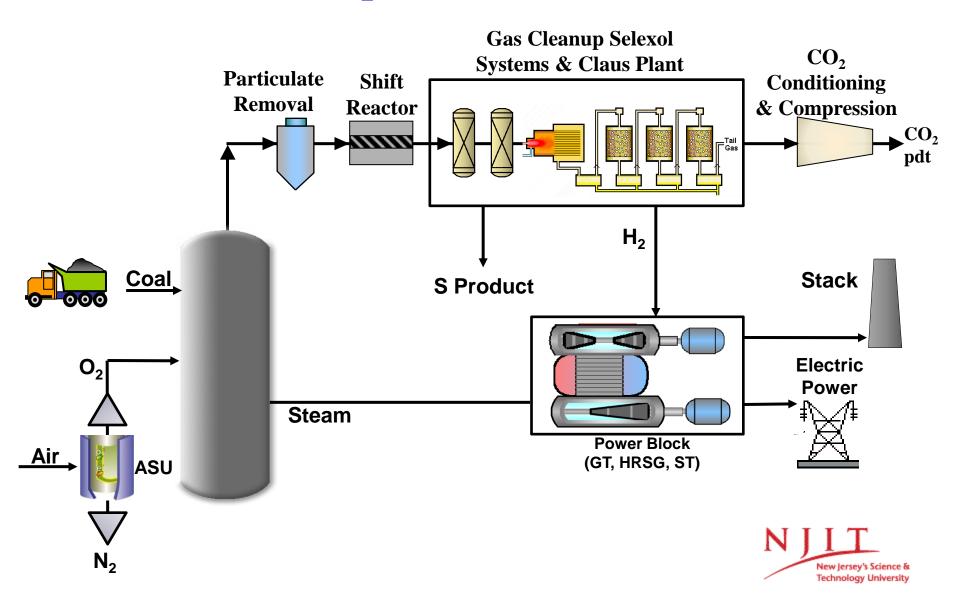
John Chau, Jie Xingming, Gordana Obuskovic, and Kamalesh K. Sirkar

Otto H. York Department of Chemical, Biological and Pharmaceutical Engineering
New Jersey Institute of Technology
Newark, NJ 07102

DOE-NETL Award No. DE-FE0001323 2010 CO₂ Capture Technology R&D Meeting Pittsburgh, September 17, 2010



Typical IGCC Plant with a Shift/Selexol based CO₂ Capture System



- Background
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- Project Objectives
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Precombustion CO₂ Capture from Shifted Syngas

- 1. Typical IGCC plant will employ Selexol-based CO₂ capture:
 - Shifted syngas is cooled, humidified and expanded to recover some energy
 - Double-stage Selexol unit will remove H₂S and CO₂
 - H₂S recovered as elemental sulfur in a Claus unit
 - CO₂ flashed off the absorbent liquid at a lower pressure (~50 psia)
- 2. Variety of Sorbent-based Process, Ca-based, Hydrotalcite-based etc., Thermal swing sorption-enhanced reaction (TSSER), PSA

Technology University

3. Membrane Processes:

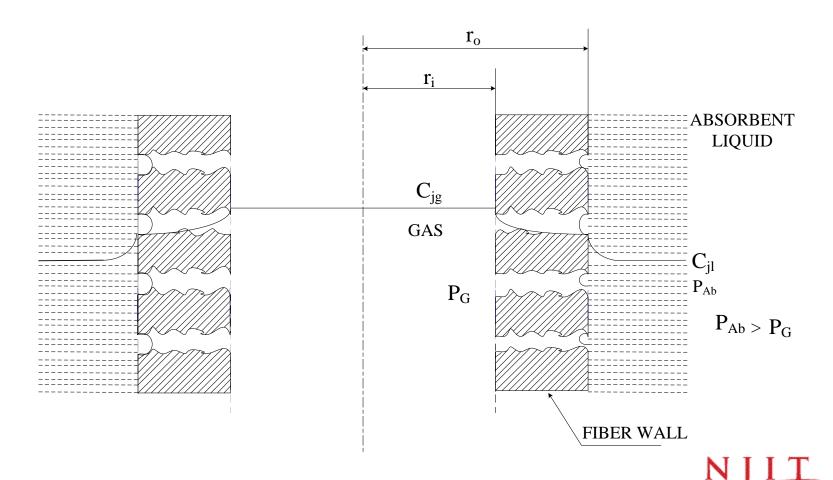
- Highly H₂-selective metallic or ceramic or zeolitic membranes
- CO₂-selective polymeric membranes
- Membrane reactor for shift gas reaction with CO₂-selective membrane
- Ionic liquid-based supported liquid membranes
- 4. Pressure swing absorption of CO₂ for post lowtemperature shift reactor gas using membrane contactors containing ionic liquids, dendrimers etc.
- 5. Other processes...



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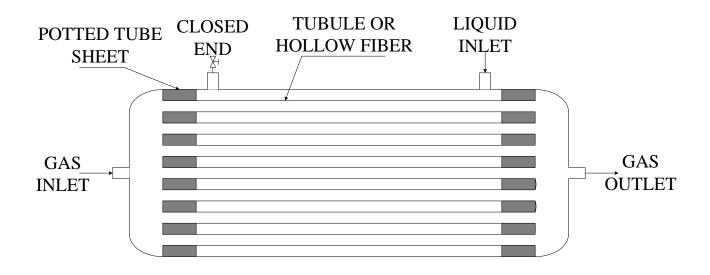


Concentration profile for absorbed species in gas and liquid phases in a membrane contactor



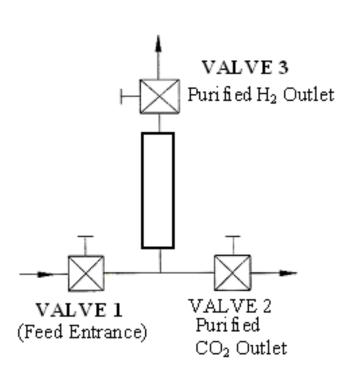
New Jersey's Science & Technology University

Schematic of the absorber containing ceramic tubules or hollow fibers

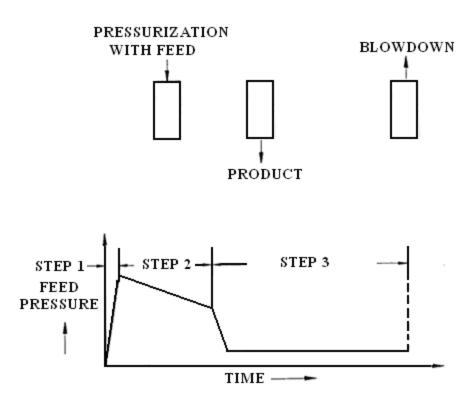




Pressure Swing Absorption Operation



Solenoid Valve Locations in Pressure Swing Absorption (PSAB) Apparatus



Pressure vs. time profile in the bore of tubule or hollow fiber in PSAB



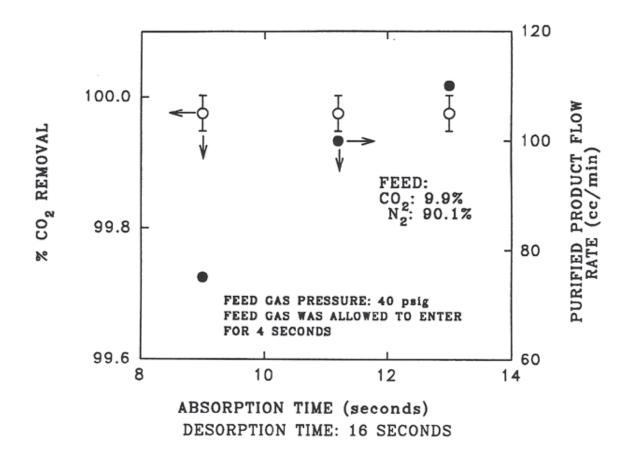
Pressure Swing Absorption (PSAB) in a Membrane Contactor Device

 Basic separation concept implemented with 10% CO₂-90% N₂ gas mixture at 375 kPa and 19.5 wt% aqueous DEA solution (RAPSAB – Rapid Pressure Swing Absorption)

• Its adaptation to the current problem of treating low temperature post-shift reactor synthesis gas at ~20 atm and 150-200°C

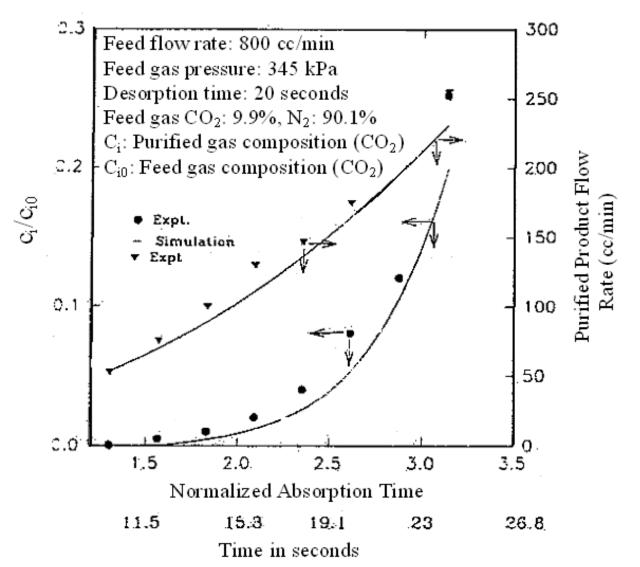


Experimental results for RAPSAB using DEA solution as an absorbent





Removal of CO₂ with DEA as an absorbent: experimental results vs. theoretical simulations



Technology University

Potential Advantages of the Proposed Separation Technique-1

- Has high solubility selectivity of novel selected liquid absorbents having relatively high viscosity
- Has high purification ability of pressure swing adsorption process
- Has high gas-liquid contacting surface area per unit device volume
- Has a compact membrane-like device
- Scale up should be easier due to modularity of membrane-based devices and membrane-based phase contacting



Potential Advantages of the Proposed Separation Technique-2

• Will deliver highly purified H₂ at nearly its partial pressure and temperature in the postshifted reactor synthesis gas feed

• Purified CO₂ stream (>90% CO₂) will be available at 1-5 atm



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Nonvolatile Absorbents for PSAB

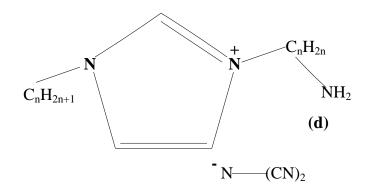
1. Ionic Liquids:

[bmim]⁺[PF₆]⁻ (Fluka)

[bmim]⁺[DCA]⁻ (Merck)

[Am-Im]⁺[DCA]⁻ (Functionalized)

(with or without moisture)



(d) Functionalized IL structure for [Am-Im]⁺[DCA]⁻

$$\mathsf{Tf_2N}^{\scriptsize \bigcirc} = \begin{array}{c} \mathsf{O} & \mathsf{O} & \mathsf{O} \\ \mathsf{O} \\ \mathsf{O} & \mathsf{O} \\ \mathsf{O} \\ \mathsf{O} & \mathsf{O} \\ \mathsf{O} \\$$

General structures of (a) imidazolium-based RTILs, (b) $[C_2mim][X]$ RTILs, and (c) $[Rmim][Tf_2N]$ RTILs. (Bara et al., *Ind. Eng. Chem. Res.*, <u>48</u>, 2739 (2009))



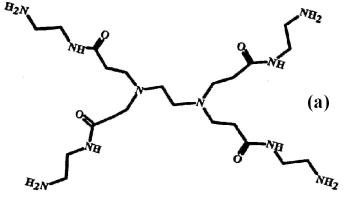
Nonvolatile Absorbents for PSAB

2.(a) Dendrimers/hyperbranched polymers of lower molecular weight:

Polyamidoamine (PAMAM) generation 0, MW-516, 4 primary

amines, 2 tertiary amines;

Generation 2, MW-3130 (Dendritech, Midland, MI) Use in a nonvolatile solvent, such as polyethylene glycol (PEG



such as polyethylene glycol (PEG 400) (a) PAMAM dendrimer of generation 0 Highly reactive in the presence of moisture

- (1. Kovvali et al., *JACS*, <u>122</u> (31) 7594 (2000); 2. Kovvali and Sirkar, *I&E C Res.*, <u>40</u>(11), 2502 (2001); 3. Kosaraju et al., *I&E C Res.*, <u>49</u>, 1250 (2005))
- (b) Polyethyleneimines of lower molecular weight, Lupasol FG (BASF), MW-615 (Rolker et al., *I&E C Res.*, <u>46</u>, 6572 (2007)

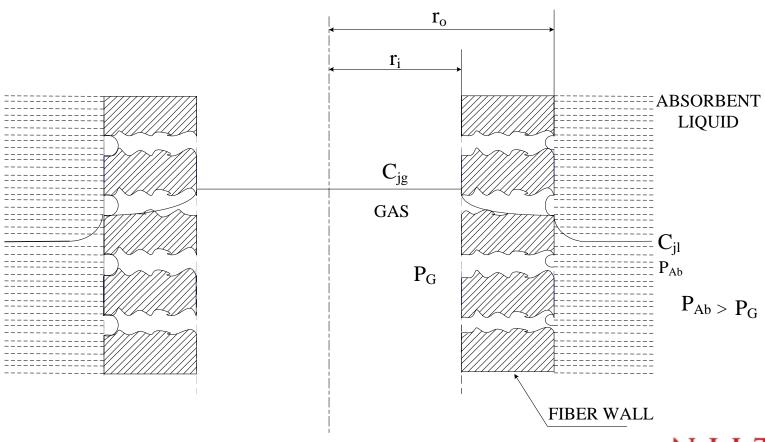


Adaptation of PSAB Device to the Current Problem

- 1. Porous PP membrane substrate replaced by hydrophobized porous ceramic tubules, porous PTFE hollow fibers and hydrophobized PEEK hollow fibers (higher temperature, wettability considerations)
- 2. High pressure means smaller membrane pore size (5 nm to 10 nm) at the gas-liquid interface to prevent any phase breakthrough
- 3. Longer length of hollow fibers in RAPSAB replaced by number of ceramic tubules in series (limitation of oven dimensions)



Concentration profile for absorbed species in gas and liquid phases





Breakthrough pressure for a nonwetted pore size of radius r_p (Young-Laplace Equation)

$$\Delta P_{breakthrough} \cong \frac{2\gamma \cos \theta}{r_p}$$

Increase γ , decrease r_p The pores should remain nonwetted.



Nondisperssive Gas Absorption/Stripping Requires Nonwetted Pores

1. To prevent spontaneous pore wetting

Surface tension of absorbent liquid

 $\gamma > \gamma_{critical}$ of the polymeric coating

- 2. $\gamma_{critical}$ of fluoropolymers, C_{18} surfaces....15-20 dyne/cm
- 3. Absorbent liquids under consideration have considerably higher γ values; γ will fluctuate due to absorption and desorption of moisture



Surface Tension / Interfacial Tension

1.
$$\gamma = \gamma_{20^{0}C} (\rho/\rho_{20^{0}C})^{4}$$

Hasse et al., J. Chem. Eng. Data, <u>54</u>, 2576 (2009).

[EMIM][MeOHP₂] etc.

Density decreased by about 0.05-0.1 gm/cm³ over 100⁰C; density in the range of 1.05-1.35 gm/cm³

- 2. Galan Sanchez et al., Trans. I. Chem. E.,Part A, *Chem. Engg. Res. & Dev.*, <u>85</u> (A1), 31 (2007)
 - \rightarrow 40-45 mN/m for [bmim]⁺[BF₄]
- 3. Klomfar et al., *J. Chem. & Engg. Data*, <u>54</u>, 1389 (2009) $[C_n mim][PF_6] \rightarrow \gamma$ decreasing from around 50 mN/m for C_3 to 36 mN/m at C_8
- 4. PAMAM dendrimer of generation $0 \rightarrow 55$ mN/m at 25° C (Kosaraju et. Al., *I* & *E* C Res., <u>44</u>, 1250 (2005)

Ceramic Tubules:

1.5 mm I.D., 3.8 mm O.D. γ-alumina coating on alpha-alumina substrate hydrophobized with nonafluorohexylsilane coating Pore radius ~5 nm <0.03μm, 940 m²/m³ surface area/device volume For say, a 40 dyne/cm liquid to withstand 20 atm+, 10 nm pore size C₁₈ hydrophobic coatings and epoxy-based tube sheet up to 200°C (Media and Process Technology, Pittsburgh, PA; Rich Ciora/Paul K.T. Liu)

• Teflon Hollow Fibers:

0.53 mm I.D., 1.08 mm O.D. Pore size <0.1 μ m Plasma polymerize a nanoporous fluorosilicone coating to reduce the pore size to $\leq 0.01 \mu$ m

(Applied Membrane Technologies, Inc., Minnetonka, MN; Stephen Conover)

PEEK Hollow Fibers:

300 μm I.D., 500 μm O.D., porous hollow fibers of poly (ether ether ketone), hydrophobized surface via fluorination of the surfaces (Porogen Inc., Woburn, MA; Ben Bikson)



M&P ceramic membrane tubes: 2" and 4" commercial elements





CO₂ Gas-Liquid/Liquid-Gas Mass Transfer Aspects

- Stagnant highly viscous absorbent liquid on the shell side
- Tube-side flowing gas present in pores of membrane

Rate of physical gas absorption
$$\alpha \sqrt{\frac{D_{CO_2}}{\pi t}}$$

Amount absorbed per unit area $\alpha \sqrt{\frac{D_{CO_2}t}{\pi}}$
 $D_{CO_2} \alpha \frac{1}{\mu_{absorbent}}$

• High temperature of operation will reduce $\mu_{absorbent}$ drastically

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Gas Mixture to be Studied

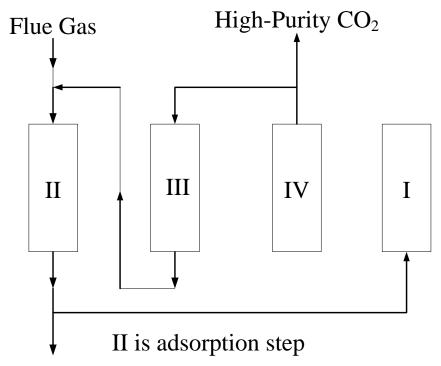
- 45% He, 30% CO₂, Rest being H₂O
- 150-200°C, 200-300 psig
- Helium as a surrogate for H₂

Typical Gasifier Composition:

~38% H₂, 29% CO₂, 33% H₂O, 0.15% CO



Concentration and Recovery of CO₂ from Flue Gas by Pressure Swing Adsorption



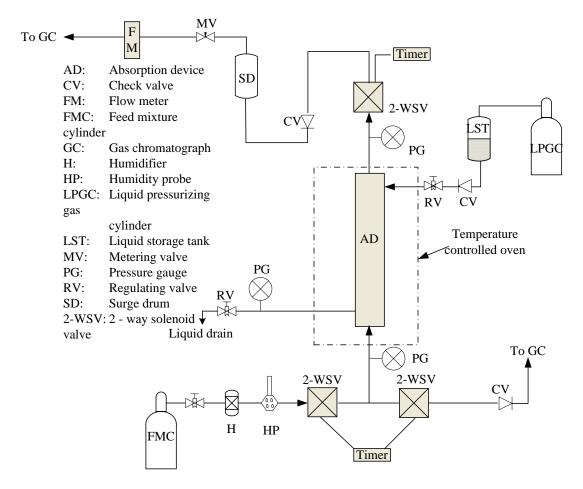
III is purge with concentrated CO₂ step

IV is countercurrent blowdown

I is pressurization with adsorption product step

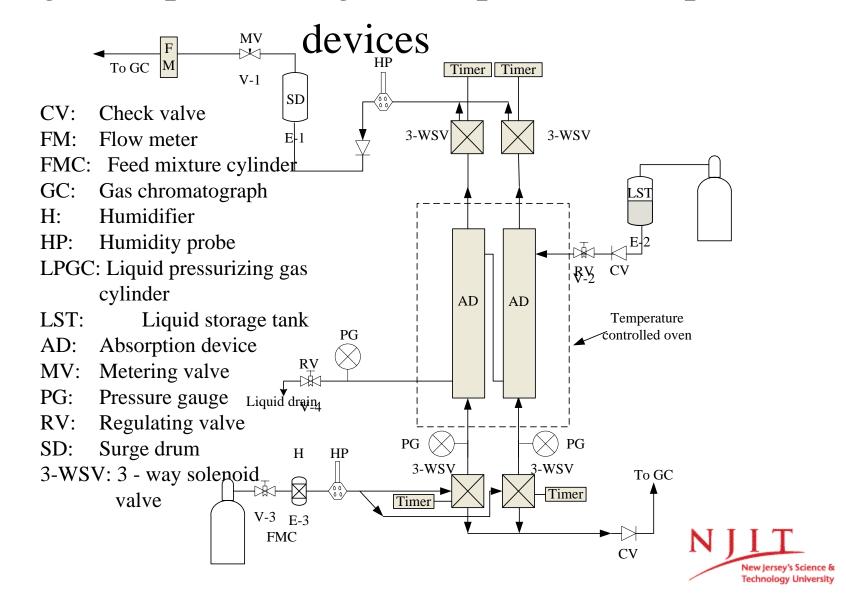


Schematic of the experimental setup for pressure swing absorption

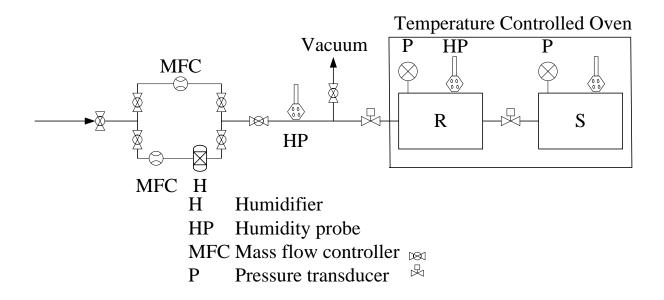




Schematic of the experimental setup for pressure swing absorption using two separate absorption



Schematic of the measurement of gas uptake by an absorbent liquid





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Project Objectives

- Develop via laboratory experiments an advanced pressure swing absorption-based device and a cyclic process to produce purified helium (a surrogate for hydrogen) at a high pressure for IGCC-CCS plant's combustion turbine from low temperature post-shift reactor synthesis gas and simultaneously obtain a highly purified CO₂ stream containing at least 90% of the CO₂ in the post-shift reactor gas stream and suitable for subsequent sequestration
- Provide data and analysis of the cyclic process and device to facilitate subsequent scale up
- Develop a detailed analysis for the process and device to allow economic evaluation for potential larger-scale use

Project Objectives: PHASE-I

- I1. Develop an experimental setup for studying the PSAB process
- **I2.** Develop novel gas-liquid absorption modules employing ceramic tubules and polymeric hollow fibers of PTFE
- **I3.** Initiate preliminary studies of pressure swing absorption-based separation of a moist CO₂-He gas mixture at 150-200°C and 200-300 psig simulating a low temperature post-shift reactor synthesis gas stream

Project Objectives: PHASE-II

- II1. Study the performance of the PSAB process for selected absorbents vis-à-vis purification of the feed gas stream to obtain a high pressure purified He stream and a low pressure purified CO₂ stream
- **II2.** Develop experimental setups to measure the solubility and diffusion coefficients of CO₂ and He at the appropriate ranges of temperature and pressure for selected absorbents
- **II3.** Initiate development of a mathematical model of the PSAB device and process

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Project Objectives: PHASE-III

- **III1.** Generate experimental data on the solubility and diffusion coefficient for CO₂ and He for the selected absorbents
- III2. Compare the results of simulation of the mathematical model with the observed purification and separation in the PSAB process and device for selected absorbents
- **III3.** Perform simulations of the model to explore scale up of the process to facilitate evaluation of the process
- **III4.** Determine the extent of loss/deterioration of the absorbents over extended periods of operation



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Phase I Progress Tasks to be Performed: Phase I

- Task 1.0 Project Management and Planning (10/1/09 9/30/10)
- Subtask 1.1 Provide quarterly reports at the end of every quarter as well as a Topical Report at the end of year 1 (10/1/09 9/30/10)
- Task 2.0 Experimental Program and Technical Activities for Year 1 (10/1/09 9/30/10)
- Subtask 2.1: Develop an experimental setup for studying the PSAB device and process (10/1/09 8/31/10)
- Subtask 2.2: Develop novel gas-liquid absorption modules (10/1/09 9/30/10)
- Subtask 2.3: Initiate preliminary studies of PSAB process (8/1/10 9/30/10)

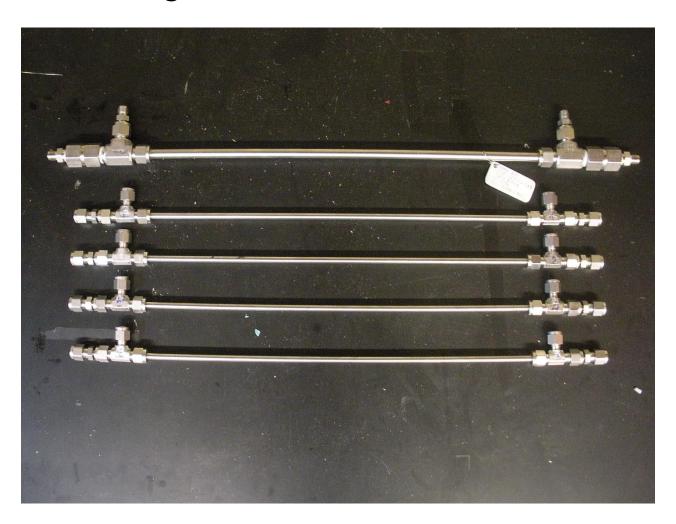


Details of Membrane Modules

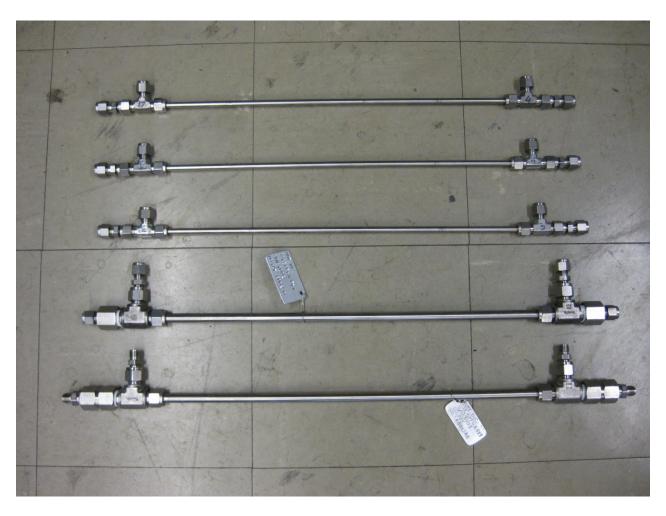
Membrane module type	Details of Membrane Modules						
	I.D. mm	O.D. mm	Pore Size μm	No. of fibers/tubules	Length	Shell Diameter	
*Ceramic membrane modules # 1,2,3,4	1.5	3.8	0.005	1	18"	1/4 " OD 0.035" wall thickness	
Teflon hollow fiber module	0.53	1.08	°0.01	18	18"	3/8" OD .035" wall thickness	
PEEK hollow fiber module	0.25	0.45	ზ.01		18"	1/4"	

^{*} Single ceramic tubule, 'o'-ring seal.

Module with Teflon Hollow Fibers and 4 Modules containing Ceramic Membrane Tubules



Ceramic Membrane Tubules in Modules and Teflon Modules



Liquid Breakthrough Pressure test results for 4 ceramic membrane modules and Teflon hollow fiber modules

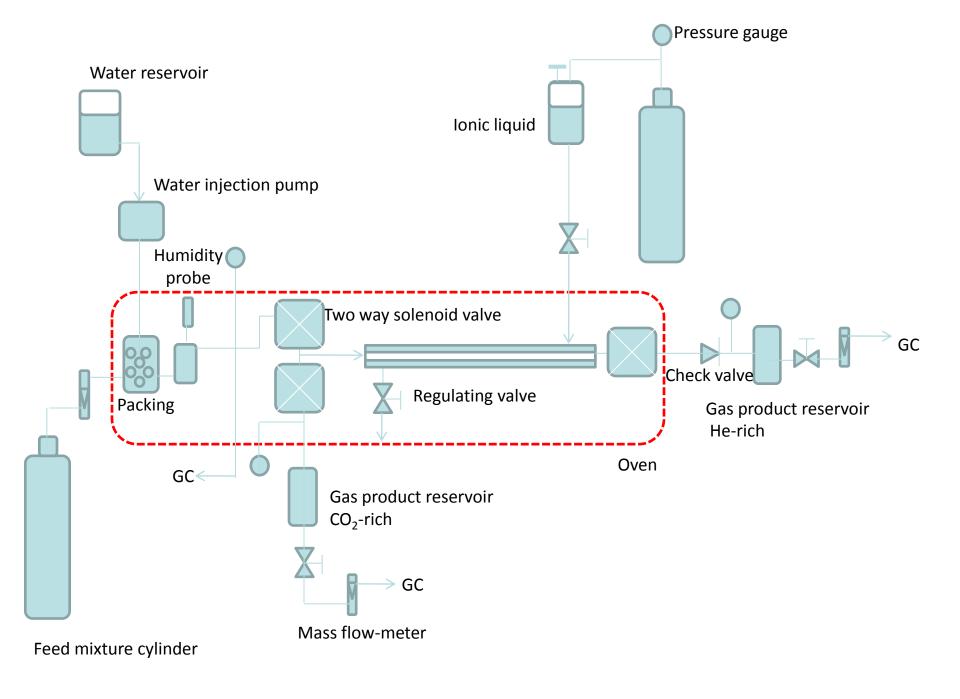
Liquid Tested Module #	Water	Glycerol Carbonate	[Bmim][DCA]	[Emim][Tf ₂ N]
*Ceramic 1	-	No leakage up to 260 psi	No leakage up to 260 psi	160 psi
*Ceramic 2	150 psi	80 psi	NA	NA
*Ceramic 3	This module may be broken	NA	NA	NA
*Ceramic 4	NA	150 psi	80 psi	NA
**Teflon	No leakage up to 80 psi	No leakage up to 80 psi	NA	NA

^{*} Single ceramic tubule; ** Tests are being done at higher pressures. Tests were carried out at room temperature.

Surface tension: Water, 72.8mN/m; Glycerol Carbonate, 45.5mN/m; [Bmim][DCA], 48.5mN/m; [Emim][Tf₂N], 41.6mN/m

ESPEC Oven Interior





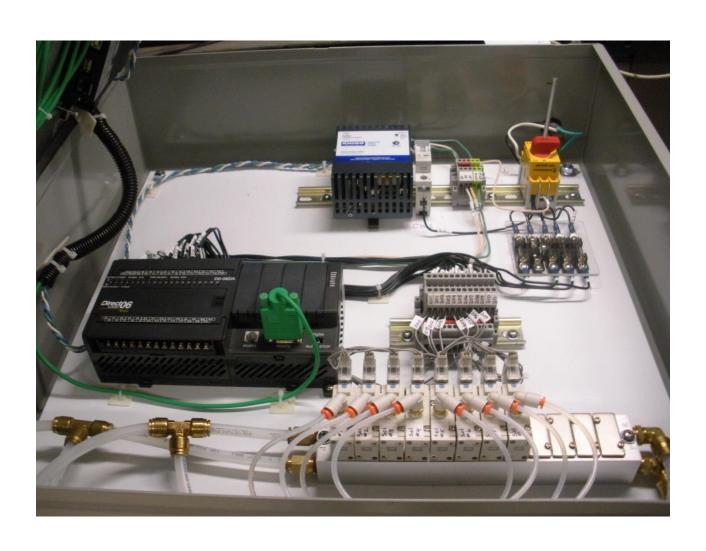
Experimental Setup inside the Oven for PSAB



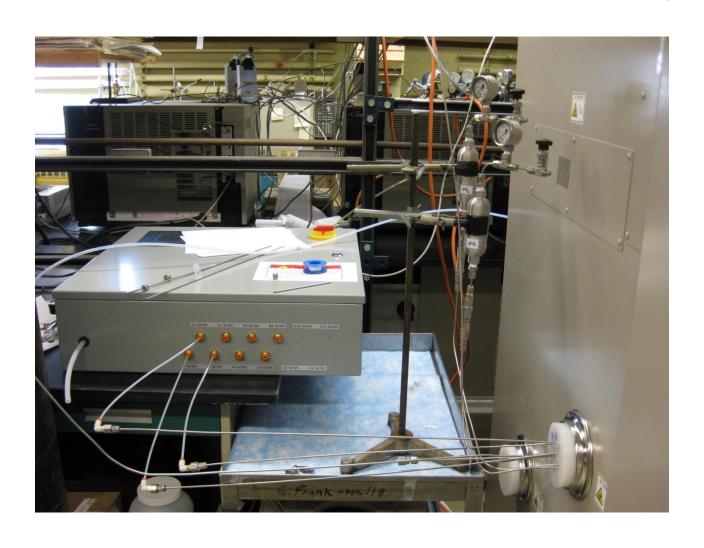
GCs



PneuMagnetic PLC Control Box



PneuMagnetic PLC Control Box with Connections to the Valves inside the Oven



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Project Structure

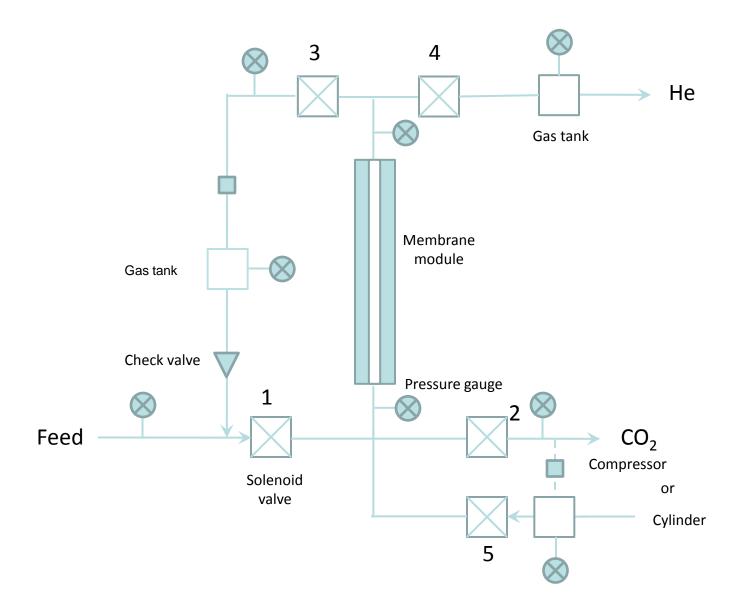
- Project Structure may be described through the List of Tasks describing in detail the following steps
- Design the device and PSAB process after selecting absorbents and the dimensions of the membrane units
- Build the setup
- Perform separation runs
- Analyze the data and focus on conditions showing the desired performance
- Develop a mathematical model for the process
- Determine the solubility and diffusivity of solutes in the absorbent liquids
- Compare model results with experimental data
- Determine absorbent deterioration with time

Tasks to be Performed: Phase II

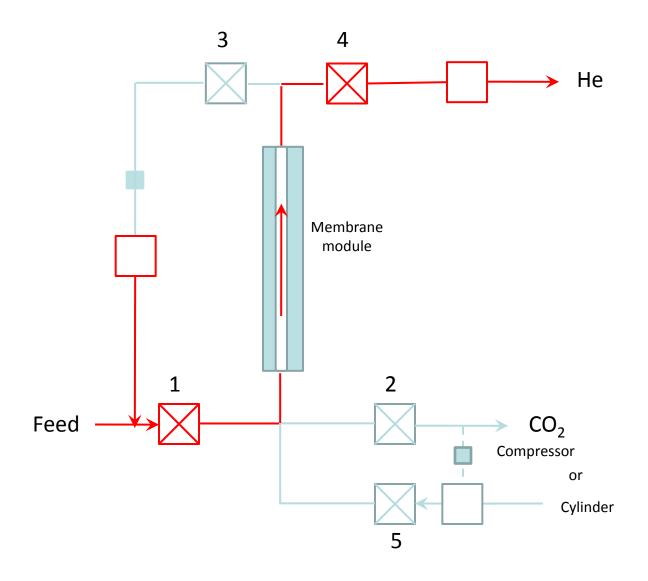
- Task 3.0 Project Management and Planning (10/1/10 9/30/11)
- Subtask 3.1 Provide quarterly reports at the end of every quarter as well as a Topical Report at the end of year 2 (10/1/10 9/30/11)
- Task 4.0 Experimental Program and Technical Activities for Year 2 (10/1/10 9/30/11)
- Subtask 4.1 Study the performance of PSAB devices and the PSAB process (10/1/10 9/30/11)
- Subtask 4.2 Develop experimental setups to measure solubility and diffusion coefficients of CO_2 and He in selected absorbent liquids (10/1/10 9/30/11)
- Subtask 4.3 Initiate development of a mathematical model of the PSAB device and process (10/1/10 9/30/11)

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One membrane module cycle



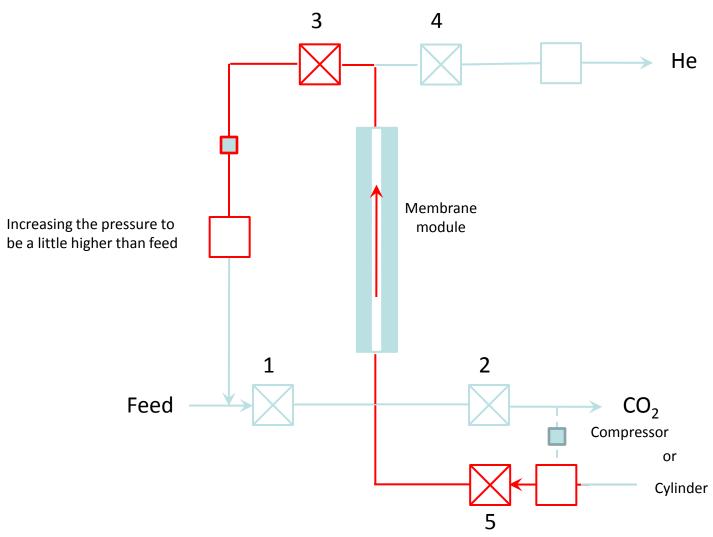
Step 1 Feed in and Absorption



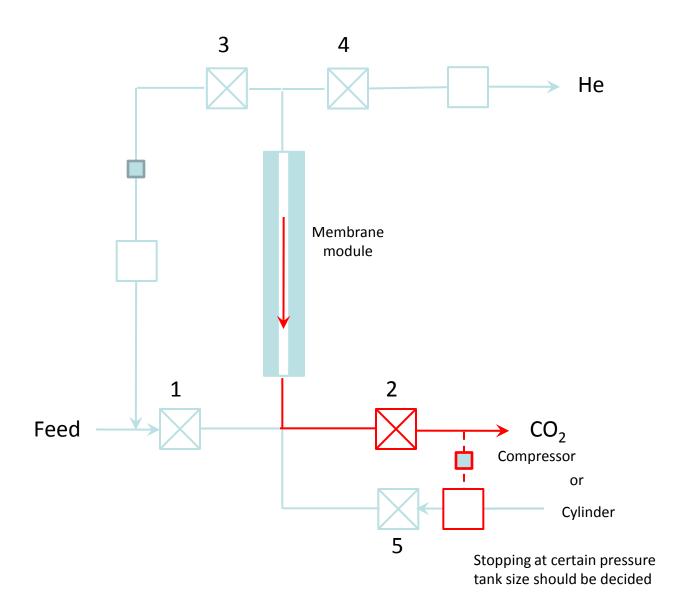
Red color means the opened line and valves

Step 2 High pressure CO₂ purge

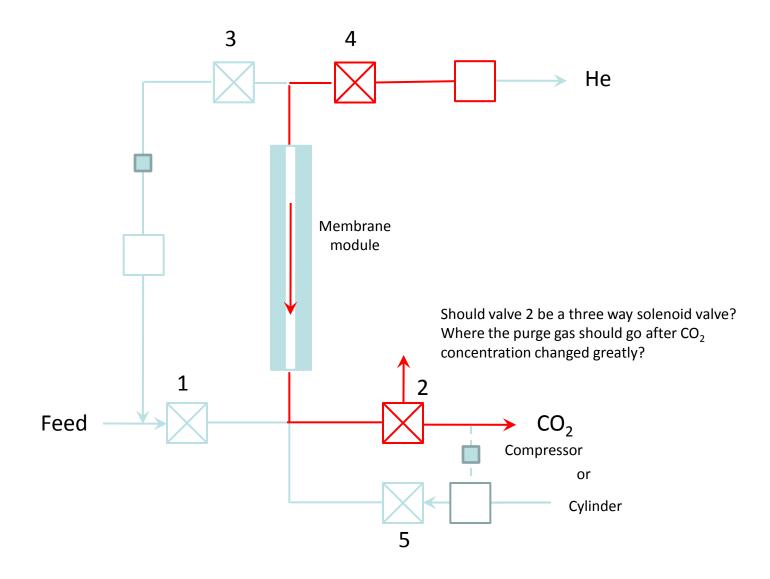
Maybe here we can collect Helium at the first several seconds?



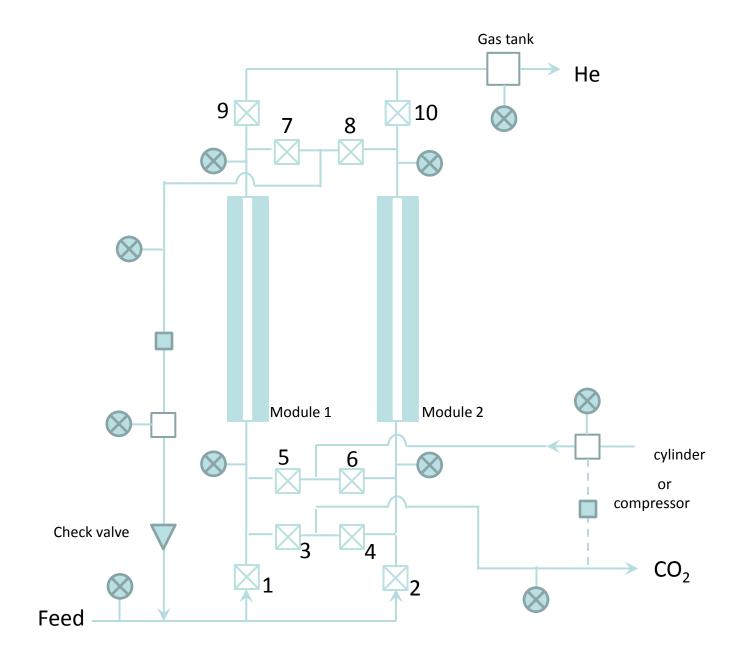
Step 3 Countercurrent blowdown



Step 4 Helium purge

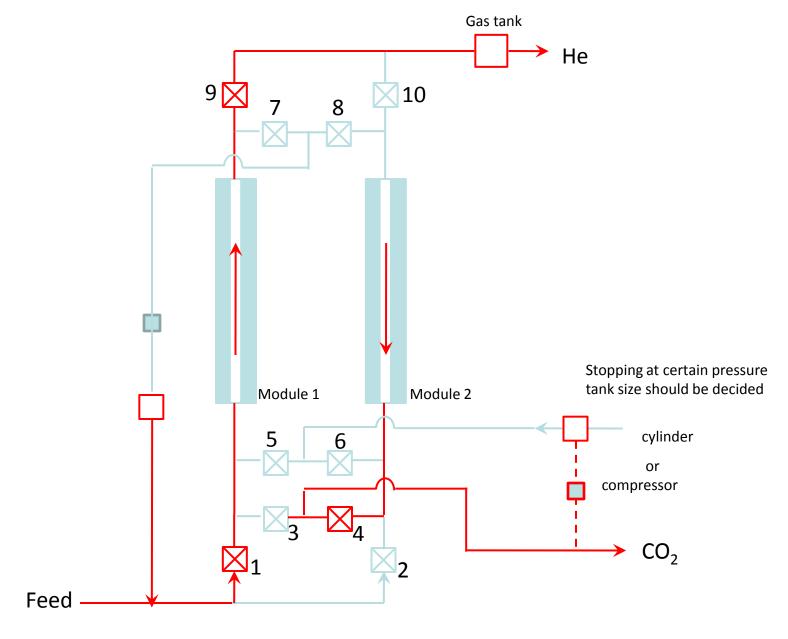


Two membrane modules cycle



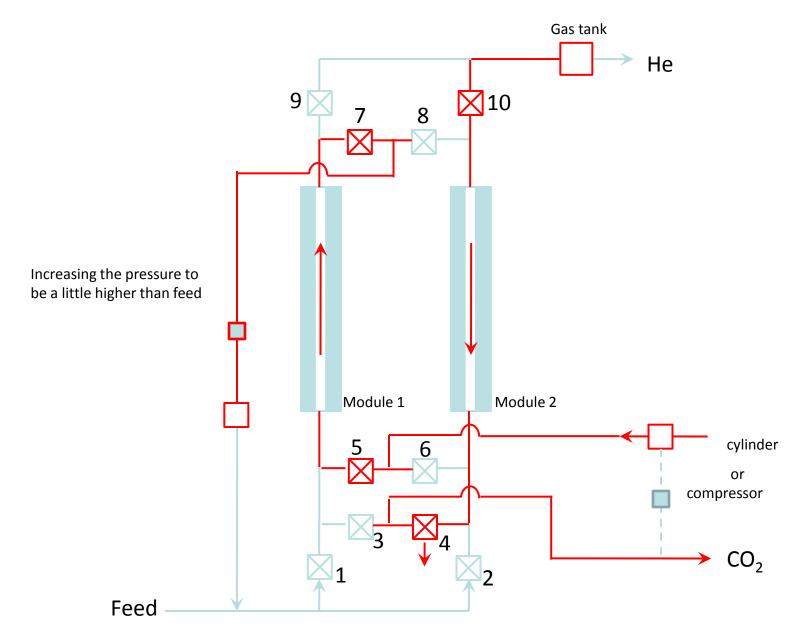
Module 1: Feed in and absorption (step 2)

Module 2: Countercurrent blowdown (step 4)



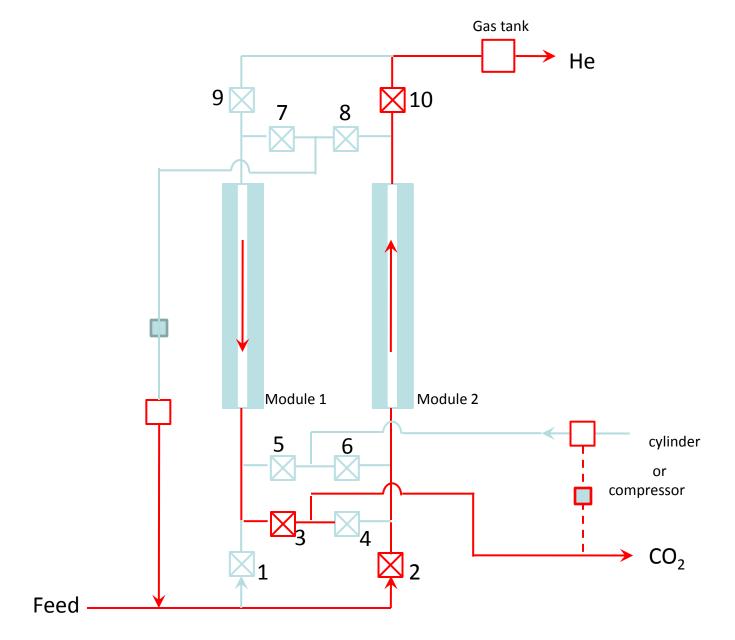
Module 1: High pressure CO₂ purge (step 3)

Module 2: Helium purge (step 1)



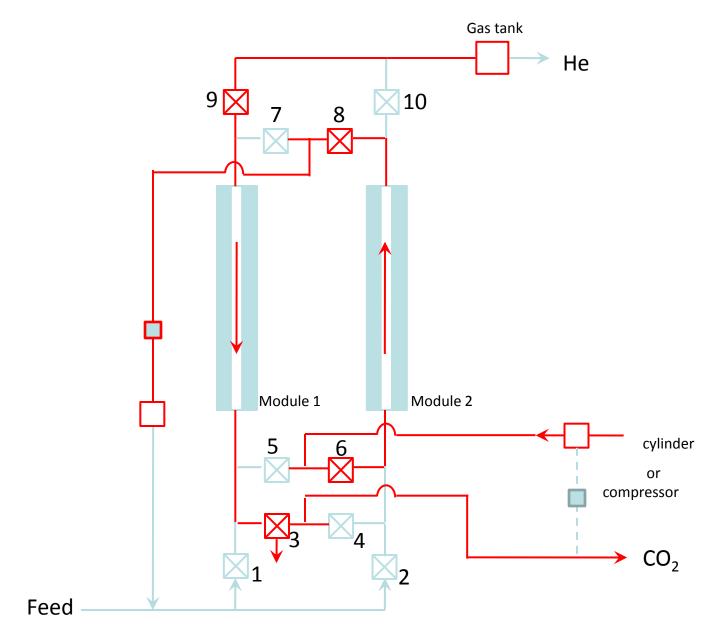
Module 1: Countercurrent blowdown (step 4)

Module 2: Feed in and absorption (step 2)



Module 1: Helium purge (step 1)

Module 2: High pressure CO₂ purge (step 3)



Tasks to be Performed: Phase III

- Task 5.0 Project Management and Planning (10/1/11 9/30/12)
- Subtask 5.1 Provide quarterly reports at the end of every quarter as well as the final Project Report at the end of year 3 (10/1/11 12/31/12)
- Task 6.0 Experimental Program and Technical Activities for Year 3 (10/1/11-9/30/12)
- Subtask 6.1 Determine the solubility and diffusivity of CO₂ and He in selected absorbents (10/1/11-6/30/12)
- Subtask 6.2 Compare mathematical model simulation results with experimental data from PSAB process (10/1/11-9/30/12)
- Subtask 6.3 Numerically explore scale up of the process to facilitate evaluation of the process (3/1/12-9/30/12)
- Subtask 6.4 Determine the loss/deterioration of the absorbents, especially amines, over extended periods (10/1/11-9/30/12)



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Project Budget

 We have spent almost all of the money budgeted for Phase I

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Project Management Plan

- Project Manager : Prof. Kamalesh K. Sirkar, PI, NJIT
- Post-Doctoral Fellow 1: Dr. Gordana Obuskovic, NJIT
- Post-Doctoral Fellow 2: Dr. Jie Xingming, NJIT
- Graduate Students: Mr. John Chau, NJIT, fully supported; Jose Sousa, limited part-time support
- Consultant : Dr. Ashok Damle, Techverse Inc., Cary, NC
- The Project Manager will interact with the following companies fabricating microporous hollow fiber membranes/tubules:
- Applied Membrane Technology, Minnetonka, MN (AMT): Stephen Conover, Thomas McEvoy, Dr. Ashok Sharma on porous hollow fiber membranes of Teflon
- Media & Process Technology, Pittsburgh, PA (M&P): Dr. Paul K.T. Liu, Richard Ciora on coating of the surfaces of ceramic tubules of alumina
- 3. Porogen Inc., Woburn, MA: Dr. Ben Bikson on porous hydrophobized PEEK hollow fiber modules

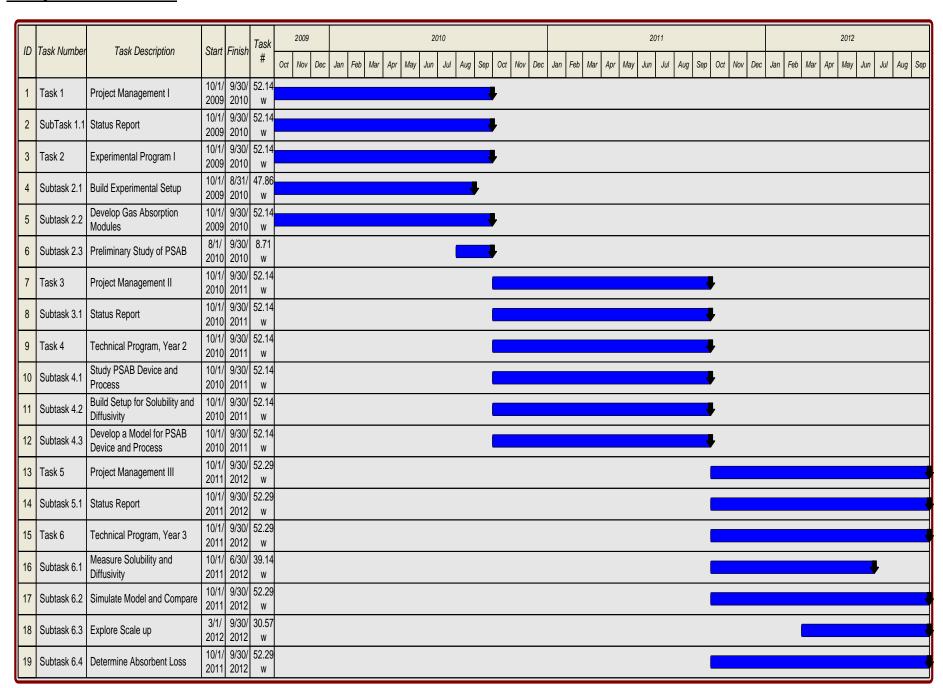
Activities of PI

- PI will work with the postdoctoral fellows (PDFs), grad. student and membrane development companies to have the membrane contactors developed
- PI will guide the PDFs and grad. student to design the system, order necessary equipment and supplies and have the set up built and tested
- PI will supervise the activities of data acquisition, device performance evaluation, estimation of properties and system modeling
- PI will lead the activities to take care of DOE reporting requirements and program review meetings
- PI will work with consultant to conduct economic evaluation of the process
- PI will make presentations and publications of results obtained from the project

Risk Management

- To prevent leakage of absorbent through microporous PTFE hollow fibers having a plasma polymerized microporous fluorosilicone coating, a finer starting pore size and a provision for leakage collection at the end of tube side
- Capability of the hydrophobic coatings on ceramic tubules to hydrophobize them sufficiently (avoid defects) to eliminate leakage of absorbent into the tube side: make provision for leakage collection at the end of tube-side and a finer starting pore size
- Effect of module diameter and length on He purification ability: smallest possible tubule diameter; increase module length by connecting them in series (oven dimension limitations)
- Achieve a steady state in the cyclic process by preventing a drift in the composition and amount of two purified product streams obtained: balance cycle between absorption and regeneration; fine tune the system

Project Timeline



Milestone Log

PHASE I

- Milestone 1: Novel absorption module fabrication successfully completed (9/30/10)
- Milestone 2: PSAB experimental setup completed (8/31/10)
- Milestone 3: PSAB device appears to function well (9/30/10)

PHASE II

- Milestone 4: PSAB device achieving high purification of He and CO₂ streams (8/31/11)
- Milestone 5: Experimental setups for measuring solubility and diffusivity completed (9/30/11)



Milestone Log

PHASE III

- Milestone 6: Mathematical Model of PSAB developed (4/30/12)
- Milestone 7: Solubilities and diffusivities of CO₂ and He measured (4/30/12)
- Milestone 8: PSAB process simulated successfully vis-à-vis experimental performance (7/31/12)
- Milestone 9: Absorbent liquid characterized and degradation determined (9/31/12)
- Milestone 10: Scaleup and economic evaluation conducted (9/31/12)



Closing Comments

- Special thanks to DOE Program Officer for the project, Norman Popkie
- We thank you for your attention
- I would be happy to respond to your questions